

#### REPORT

# RUN-ON AND RUN-OFF CONTROL SYSTEM PLAN - PERIODIC UPDATE

St. Johns River Power Park Byproduct Storage Area B Phase I Development

Submitted to:

#### St. Johns River Power Park 11201 New Berlin Road Jacksonville, Florida 32226 USA

Submitted by:

#### Golder Associates Inc.

9428 Baymeadows Road, Suite 400 Jacksonville, Florida USA 32256

+1 904 363-3430

19-124481

October 2021

### **Distribution List**

1 Copy - St. Johns River Power Park



#### **PROFESSIONAL ENGINEER CERTIFICATION**

I, Samuel F. Stafford, being a registered Professional Engineer in the state of Florida, do hereby certify to the best of my knowledge, information, and belief, that the information contained in this Run-On and Run-Off Control System Plan dated October 20, 2021 was conducted in accordance with the requirements of 40 CFR §257.81, is true and correct, and had been prepared in accordance with recognized and generally accepted good engineering practices.

Samuel F. Stafford, PE Florida Professional Engineer No. 78648 Authorization No. 1670

10/20/2021

Date



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#### APPENDIX A

#### 1.0 INTRODUCTION

In October 2016, a Run-On and Run-Off Control System (ROROCS) Plan was prepared for the Phase I development of Area B Byproduct Storage Area (Area B BSA) at the St. Johns River Power Park in Duval County, Florida, in accordance with the requirements of the federal coal combustion residual (CCR) rule. Pursuant to §257.81(c), this plan is being updated to reflect the change in conditions at Area B BSA. Specifically, this ROROCS plan documents how the facility's run-on and run-off control systems meet the requirements of §257.81 following closure of Area B BSA and includes supporting engineering calculations and modeling analysis. This Plan will be included in the facility's operating records in accordance with §257.105(g)(3).

#### 2.0 **REGULATORY REQUIREMENTS**

#### 2.1 Federal CCR Rule

The CCR Rule, 40 CFR Part 257, Subpart D, requires that the owner or operator of a new and existing CCR landfill must prepare an initial and periodic ROROCS plans which document how the run-on and run-off control systems meet the following requirements as outlined in 40 CFR 257.81(a):

- A run-on control system must prevent flow onto the active portion of the CCR unit during the peak discharge from the 25-year, 24-hour storm event.
- A run-off control system from the active portion of the CCR unit must collect and control the peak discharge from the 25-year, 24-hour storm event.

The active portion is defined by 40 CFR 257.53 as the part of the CCR unit that has received or is receiving CCR or non-CCR waste and has not completed closure in accordance with 40 CFR Part 257.102. Area B BSA has been closed and capped and no longer has an active portion.

#### 3.0 **DESIGN METHODOLOGIES**

#### 3.1 Design Storm

The existing run-on and run-off control systems were designed for hydraulic capacity for at least the 25-year, 24-hour storm event as required by local and federal regulations. Site-specific precipitation estimates were obtained from Natural Resource Conservation Service (NRCS) 24-hour rainfall maps and the Soil Conservation Service Florida Modified Type II Rainfall Distribution was used. The 25-year, 24-hour storm event generates approximately 9.0 inches of precipitation at SJRPP.

#### 3.2 Hydrologic Calculation and Stormwater Routing Methods

Hydrology calculations were completed using NRCS methods. Time of concentration values were calculated for each basin by dividing the flow paths into sheet flow and shallow concentration segments. The time of concentration calculations for the stormwater model are presented in Appendix A.

Composite curve numbers (CN) were calculated for each basin within the stormwater models (see Appendix A). CCR material was assumed to perform hydrologically consistent with bare soil conditions, which conservatively correlates to a CN of 86. Final cover material was assumed to perform hydrologically consistent with open space with good vegetative condition, which correlates to a CN of 74. A CN of 98 was used for impervious surfaces. Hydrologic soil group C was assumed for curve number computations.

Stormwater discharge and flow routing calculations were performed using the Streamline Technologies Interconnected Pond Routing (ICPR) version 4 stormwater modeling software. The ICPR model operates using three key elements that include basins, nodes, and links. The basins represent the hydrological information for each drainage contributing area. Stage-area data (or depressional storage areas) within each drainage basin was input into nodes. The nodal warning stages correlate to the maximum stage that can be reached within the depressional storage areas before overtopping occurs (e.g., top of bank elevation). The nodal warning stages vary for each drainage basin node. Nodes are interconnected by links and the links represent the existing or proposed culverts/pipes, ditches/swales, and weirs for flow routing.

#### 4.0 RUN-ON CONTROL

Run-on is defined as stormwater that may flow towards the active portion a CCR unit. Area B BSA has been capped and closed and therefore has no active portion. Furthermore, based on the topography of the Area B BSA and surrounding topography, run-on potential is low. Area B BSA is topographically higher than surrounding areas and is surrounded by berms and a network of stormwater collection areas. The perimeter berms and stormwater collection areas (ditches, swales, and ponds) would intercept run-on flows.

#### 5.0 RUN-OFF CONTROL

Run-off is defined as stormwater that falls on and flows off of Area B BSA. The CCR material has been covered with a final cover system and only non-contact stormwater will be generated. The final cover configuration of Area B BSA was analyzed for stormwater run-off management as it would generate the highest volume of stormwater run-off. At 20-foot (vertical) intervals, 2-foot deep, 10-foot-wide benches (backwardly inclined channels) have been constructed, with approximately 0.5 percent longitudinal slope that outlet to the perimeter ditch system via downcomer pipes (18-inch diameter), spaced approximately 500 feet apart. The perimeter ditch system will convey stormwater either to Pond A or Pond B via culverts. Stormwater will eventually discharge via infiltration to the water table or (under peak storm conditions) through control structures. Pond B may discharge under peak storm conditions via an overflow weir and associated channel to Pond A. Pond A will discharge under peak storm conditions via pipes and an overflow weir or control structure to an unnamed tributary of Clapboard Creek. The final cover configuration consists of 11 drainage basins and associated depressional storage areas that are interconnected by a series of pipes directing runoff ultimately to Pond B and Pond A (see Figure 1). Pond A, Pond B and the Pond A outfall location were modeled as Node 1, Node 10, and Node 7, respectively. The ICPR nodal diagram, model inputs, and results for the non-contact stormwater run-off configuration are presented in Appendix A.

The modeling results indicate that the final cover stormwater management system for Area B BSA has adequate capacity to collect, manage and route flows from the 25-year, 24-hour return period as warning stages were not exceeded at any of the basin nodes (no overtopping). The nodal peak staging results and available freeboard for each sub-area are summarized below:

Node	Description	Peak Stage (feet)	Warning Stage (feet)	Freeboard 25-year, 24-hour Storm (feet)
1	Pond A	8.97	11.00	2.03
2	Final Cover East Slope and Perimeter Ditch	12.18	12.60	0.42
3	Final Cover South Slope and Perimeter Ditch	13.8	15.00	1.2
4	Final Cover Southwest Slope and Swale	19.44	20.65	1.21
5	Final Cover Northwest Slope and Swale	16.78	18.07	1.29
6	Final Cover North Slope and Swale	12.77	13.73	0.96
9	Depressional Storage East of Pond B	12.6	14	1.4
10	Pond B	9.14	13	3.86
11	Ditch Northeast of Pond B	12.57	14	1.43

Table 1: 25-year, 24-hour Peak Stage and Freeboard Summary
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### 6.0 CLOSING

As required by 40 CFR 257.81, the Area B BSA run-on control system has the capacity to prevent flow onto the active portion of the CCR unit during the peak discharge from a 25-year, 24-hour storm, and the run-off control system has the capacity to collect, manage and route flows resulting from a 25-year, 24-hour storm.



### Signature Page

Golder Associates Inc.

Samuel F. Stafford, PE Senior Engineer

HH/SFS/DJM/as

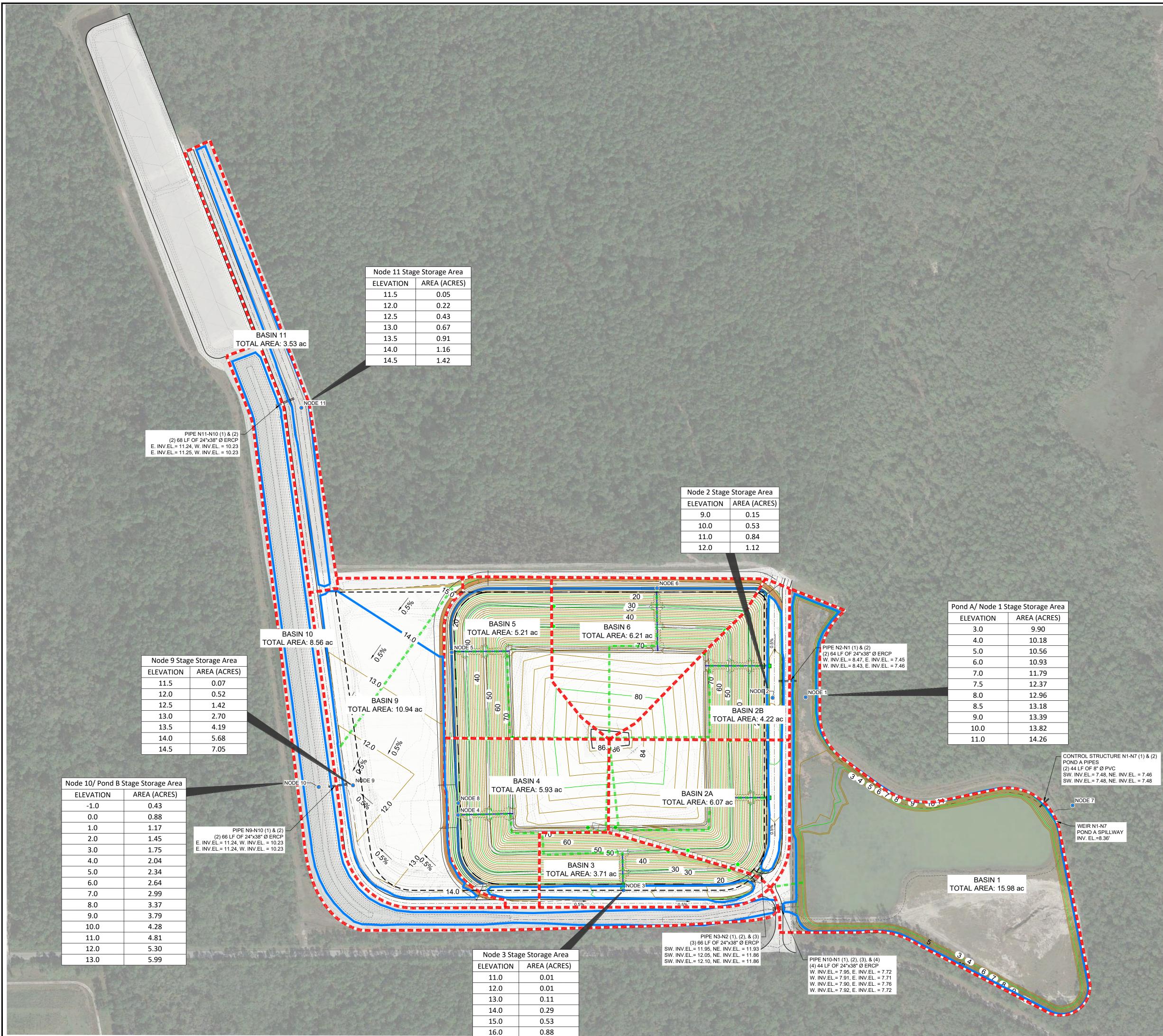
Donald J. Miller Principal and Practice Leader

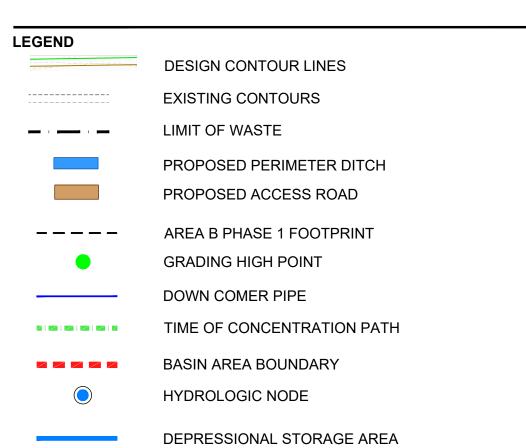
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## FIGURE





NOTE(S)

19-124481

1. PROPOSED CONTOURS REPRESENT TOP OF FINAL COVER GRADES AFTER COMPLETION OF GRADING ACTIVITIES.

JEA			
CONSULTANT		YYYY-MM-DD	2021-09-30
		DESIGNED	НН
	GOLDE	R PREPARED	BCL
	MEMBER OF WSP	REVIEWED	SFS
		APPROVED	DJM
	ND RUN-OFF COI S RIVER POWER F	NTROL SYSTEM	DJM
	-	UNTY, FLORIDA	
	S RIVER POWER P	PARK	

19124481-N002

APPENDIX A

Stormwater Run-Off Calculations and Model

#### **Time of Concentration Calculations**

Hydrology calculations were completed using NRCS methods. Time of concentration values were calculated for each basin by dividing the flow paths into different segments based on overland flow characteristics. The travel times for each flow path were summed to get a time of concentration. The flow paths were divided into the following categories:

1. <u>Sheet Flow</u> – the maximum sheet flow distance used was 300 feet. The SCS equation for overland flow using Manning's equation was used and is shown below:

$$T_t = \frac{(0.007)(n*L)^{0.8}}{P_2^{0.5}(S)^{0.4}}$$
, where:

 $T_t = Travel Time (min.)$ n = Manning's n L = Flow path length (ft.) P<sub>2</sub> = 2-year, 24-hour rainfall (in.) S = Flow path slope (ft./ft.)

2. <u>Shallow Concentrated Flow</u> –concentrated overland flow towards channels. The equation for shallow concentrated flow is shown below:

$$T_t = \frac{L}{V} * \frac{1}{60}$$
, where:

 $\begin{array}{l} T_t = Travel \mbox{ Time (min.)} \\ L = Flow \mbox{ path length (ft.)} \\ v = Flow \mbox{ velocity (feet/second)} \end{array}$ 

Time of concentration calculations for each basin are presented in Table 2.

#### **Composite Curve Number Calculations**

CCR material was assumed to perform hydrologically consistent with bare soil conditions, which correlates to runoff curve number values ranging from 77 to 94 depending on the hydrologic soil group. Final cover material was assumed to perform hydrologically consistent with Open Space, Good Condition (grass cover > 75%), which correlates to runoff curve number values ranging from 39 to 80 depending on the hydrologic soil group. Hydrologic soil group B was assumed for curve number computations.

Composite curve number calculations for each basin are presented in Table 2.

St. Johns River Power Park CURVE NUMBER & TIME OF CONCENTRATION REVISED AREA B DRAINAGE BASINS								
Basin Description 1 (Pond A) 15.98 ac.								
<u>CN:</u>								
	<u>Ac.</u>	Land Cover	Soil Type	SCS CN	<u>%</u>	Weight %		
	0.92	Tie-in Areas (Open Space - Good)	C	74	5.8%	4		
	0.00	Perimeter Road (Impervious)	-	98	0.0%	0		
	15.06	Pond/Pool (Water)	-	98	94.2% 100.0%	92		
Total:	15.98	<u>OK</u>		Weighted S	SCS CN =	97		
		segment less than 300-ft was calculated using						
First Time of The second s The remainin Mannings of t	segment was ca ng segment was 0.24 - Dense G	lculated using the TR-55 velocity vs. slope cri calculated using average channel flow veloci rasses	teria for shallo by obtained from	w concentrate	ed flow			
<sup>•</sup> First Time of <sup>•</sup> The second s <sup>•</sup> The remainin <sup>•</sup> Mannings of ( <sup>•</sup> P2-yr,24-hr (i	segment was ca ng segment was 0.24 - Dense G in.) - NOAA Pre	Iculated using the TR-55 velocity vs. slope cri calculated using average channel flow veloci rasses cipitation Frequency Data Server for Jackson	teria for shallo by obtained from	w concentrate	ed flow			
First Time of The second s The remainin Mannings of 0 P2-yr,24-hr (i Overland	segment was ca og segment was 0.24 - Dense G in.) - NOAA Pre Mannings n	Iculated using the TR-55 velocity vs. slope cri calculated using average channel flow velocit rasses cipitation Frequency Data Server for Jacksonv P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	teria for shallo ty obtained fro ville, FL	w concentrate	ed flow			
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i	segment was ca og segment was 0.24 - Dense G in.) - NOAA Pre Mannings n	Iculated using the TR-55 velocity vs. slope cri calculated using average channel flow veloci rasses cipitation Frequency Data Server for Jackson	teria for shallo ty obtained fro ville, FL	w concentrate	ed flow			
First Time of The second s The remainin Mannings of 0 P2-yr,24-hr (i Overland	segment was ca og segment was 0.24 - Dense G in.) - NOAA Pre Mannings n	Iculated using the TR-55 velocity vs. slope cri calculated using average channel flow velocit rasses cipitation Frequency Data Server for Jacksonv P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	teria for shallo ty obtained fro ville, FL	w concentrate	ed flow	Time (min.)	<u>.</u>	
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i Overland	segment was ca ng segment was 0.24 - Dense G in.) - NOAA Pre Mannings n 0.24	Iculated using the TR-55 velocity vs. slope cri calculated using average channel flow velocit rasses cipitation Frequency Data Server for Jacksonv P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	teria for shallo ty obtained fro ville, FL	w concentrate m Channel De	ed flow	<u>Time (min.)</u> 8	<u>1</u>	
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i Overland	segment was ca ng segment was 0.24 - Dense G in.) - NOAA Pre Mannings n 0.24 <u>Dist. (ft)</u>	Iculated using the TR-55 velocity vs. slope cri calculated using average channel flow velocit rasses cipitation Frequency Data Server for Jacksonv P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.) 4.74 0.05	teria for shallo ty obtained fro ville, FL	w concentrate m Channel De	ed flow		<u>.</u>	
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i Overland	segment was ca og segment was 0.24 - Dense G in.) - NOAA Pre Mannings n 0.24 <u>Dist. (ft)</u> 100	Iculated using the TR-55 velocity vs. slope criticalculated using average channel flow velocity rasses   cipitation Frequency Data Server for Jackson   P2-yr,24-hr (in.)   Slope (ft./ft.)   4.74   0.05	teria for shallo ty obtained from /ille, FL	w concentrate m Channel De <u>Vel. (fps)</u>	ed flow	8	<u>l</u>	

St. Johns River Power Park CURVE NUMBER & TIME OF CONCENTRATION REVISED AREA B DRAINAGE BASINS								
Basin Description2A6.07 ac.								
<u>CN:</u>								
	Ac.	Land Cover	<u>Soil Type</u>	SCS CN	<u>%</u>	Weight %		
	<u>Ac.</u> 5.32	Final Cover (Open Space - Good)	С	74	87.6%	65		
	0.34	Perimeter Road (Impervious)	-	98	5.6%	5		
	0.41	Pond/Pool (Water)	-	98	6.8% 100.0%	7		
Total:	6.07	<u>OK</u>		Weighted S	SCS CN =	77		
<b>Tc:</b> First Time of	Concentration s	egment less than 300-ft was calculated using	g the TR-55 for	mula for sheel	flow			
*First Time of *The second s *The remainin	egment was ca	Iculated using the TR-55 velocity vs. slope cr calculated using average channel flow veloci	iteria for shallo	w concentrate	d flow			
First Time of The second s The remaining Mannings of (	egment was ca g segment was 0.24 - Dense Gr	lculated using the TR-55 velocity vs. slope cr calculated using average channel flow veloci asses	iteria for shallo ty obtained froi	w concentrate	d flow			
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Preo	Iculated using the TR-55 velocity vs. slope cr calculated using average channel flow veloci asses cipitation Frequency Data Server for Jackson	iteria for shallo ty obtained froi	w concentrate	d flow			
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Preo Mannings n	Iculated using the TR-55 velocity vs. slope cr calculated using average channel flow veloci asses cipitation Frequency Data Server for Jackson	iteria for shallo ity obtained froi ville, FL	w concentrate	d flow			
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i Overland	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Pred Mannings n 0.24	Iculated using the TR-55 velocity vs. slope or calculated using average channel flow veloci rasses cipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	iteria for shallo ity obtained froi ville, FL	w concentrate	d flow	Time (min.)		
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i Overland	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Preo Mannings n	Iculated using the TR-55 velocity vs. slope or calculated using average channel flow veloci rasses cipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	iteria for shallo ity obtained froi ville, FL	w concentrate m Channel De	d flow	<u>Time (min.)</u> 20		
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i Overland	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Pred Mannings n 0.24 <u>Dist. (ft)</u>	Iculated using the TR-55 velocity vs. slope or calculated using average channel flow veloci asses cipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.) 4.74 0.05	iteria for shallo ity obtained froi ville, FL	w concentrate m Channel De	d flow			
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i Overland	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Pred Mannings n 0.24 <u>Dist. (ft)</u> 300	Iculated using the TR-55 velocity vs. slope or calculated using average channel flow velocitasses   cipitation Frequency Data Server for Jackson   P <sub>2-yr,24-hr</sub> (in.)   Slope (ft./ft.)   4.74   0.05	iteria for shallo ity obtained froi ville, FL	w concentrate m Channel De <u>Vel. (fps)</u>	d flow	20		
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i Overland	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Pred Mannings n 0.24 <u>Dist. (ft)</u> 300 30	Iculated using the TR-55 velocity vs. slope or calculated using average channel flow velocitasses   cipitation Frequency Data Server for Jackson   P2-yr,24-hr (in.) Slope (ft./ft.)   4.74 0.05   Sheet Flow   Shallow concentrated flow	iteria for shallo ity obtained froi ville, FL	w concentrate m Channel De <u>Vel. (fps)</u> <u>3.61</u>	d flow	20 0		

St. Johns River Power Park CURVE NUMBER & TIME OF CONCENTRATION REVISED AREA B DRAINAGE BASINS								
Basin Description2B4.22 ac.								
<u>CN:</u>								
	<u>Ac.</u>	Land Cover	Soil Type	SCS CN	<u>%</u>	<u>Weight %</u>		
	3.46	Final Cover (Open Space - Good)	C	74	82.0%	61		
	0.34	Perimeter Road (Impervious)	-	98	8.1%	8		
	0.42	Pond/Pool (Water)	-	98	10.0% 100.0%	10		
Total:	4.22	<u>OK</u>		Weighted S		78		
*The remaining	-	culated using the TR-55 velocity vs. slope cr calculated using average channel flow veloci asses						
P2-vr 24-hr (ir		pipitation Frequency Data Server for Jackson	<u>/</u> ille, FL					
Overland I	Mannings n	P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)						
		P <sub>2-yr,24-hr</sub> (in.)   Slope (ft./ft.)     4.74   0.05	1					
Overland I			]	<u>Vel. (fps)</u>		<u>Time (min.)</u>		
Overland [	0.24		]	<u>Vel. (fps)</u>		<u>Time (min.)</u> 20		
Overland [	0.24 <u>Dist. (ft)</u>	4.74 0.05	_	<u>Vel. (fps)</u> 3.61				
Overland [	0.24 <u>Dist. (ft)</u> 300	4.74 0.05 Sheet Flow	]			20		

St. Johns River Power Park CURVE NUMBER & TIME OF CONCENTRATION REVISED AREA B DRAINAGE BASINS								
Basin Description33.71 ac.								
<u>CN:</u>								
	<u>Ac.</u>	Land Cover	<u>Soil Type</u>	SCS CN	%	Weight 9	6	
	2.57	Final Cover (Open Space - Good)	С	74	69.3%	51		
	0.51	Perimeter Road (Impervious)	-	98	13.7%	13		
	0.63	Pond/Pool (Water)	-	98	17.0%	17		
					100.0%			
Total:	3.71	<u>OK</u>		Weighted S	SCS CN =	81		
		segment less than 300-ft was calculated usin alculated using the TR-55 velocity vs. slope c	-					
First Time of ( The second s The remaining Mannings of ( P2-yr,24-hr (ir	egment was c g segment wa 0.24 - Dense C	alculated using the TR-55 velocity vs. slope c s calculated using average channel flow veloc Grasses ecipitation Frequency Data Server for Jacksor	riteria for shallo hity obtained from	w concentrate	d flow			
First Time of ( The second s The remaining Mannings of ( P2-yr,24-hr (ir	egment was c g segment wa 0.24 - Dense C n.) - NOAA Pro Mannings n	alculated using the TR-55 velocity vs. slope c s calculated using average channel flow veloc Grasses ecipitation Frequency Data Server for Jacksor	riteria for shallo ity obtained froi nville, FL	w concentrate	d flow			
First Time of 0 The second s The remaining Mannings of 0 P2-yr,24-hr (ir Overland	egment was c g segment wa 0.24 - Dense ( n.) - NOAA Pro Mannings n 0.2	alculated using the TR-55 velocity vs. slope c s calculated using average channel flow veloc Grasses ecipitation Frequency Data Server for Jacksor P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	riteria for shallo ity obtained froi nville, FL	w concentrate m Channel De	d flow	Time (mii	1.)	
First Time of ( The second s The remaining Mannings of ( P2-yr,24-hr (ir Overland	egment was c g segment wa 0.24 - Dense C n.) - NOAA Pro Mannings n	alculated using the TR-55 velocity vs. slope c s calculated using average channel flow veloc Grasses ecipitation Frequency Data Server for Jacksor P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	riteria for shallo ity obtained froi nville, FL	w concentrate	d flow	<u>Time (mii</u> 3	<u>ı.)</u>	
First Time of ( The second s The remaining Mannings of ( P2-yr,24-hr (ir Overland	egment was c g segment wa 0.24 - Dense C n.) - NOAA Pro Mannings n 0.2 <u>Dist. (ft)</u>	alculated using the TR-55 velocity vs. slope c s calculated using average channel flow veloc Grasses ecipitation Frequency Data Server for Jacksor P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.) 4 4.74 0.33	riteria for shallo ity obtained froi nville, FL	w concentrate m Channel De	d flow		<u>ı.)</u>	
First Time of ( The second s The remaining Mannings of ( P2-yr,24-hr (ir Overland	egment was c g segment wa: 0.24 - Dense C n.) - NOAA Pro Mannings n 0.2 <u>Dist. (ft)</u> 75	alculated using the TR-55 velocity vs. slope c s calculated using average channel flow veloc Grasses ecipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.) 4 4.74 0.33	riteria for shallo ity obtained froi nville, FL	w concentrate m Channel De <u>Vel. (fps)</u>	d flow	3	<u>ı.)</u>	
First Time of ( The second s The remaining Mannings of ( P2-yr,24-hr (ir Overland Flow	egment was c g segment wa 0.24 - Dense C n.) - NOAA Pro Mannings n 0.2 <u>Dist. (ft)</u> 75 0 285	alculated using the TR-55 velocity vs. slope c s calculated using average channel flow veloc Grasses ecipitation Frequency Data Server for Jacksor P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.) 4 4.74 0.33 Sheet Flow Shallow concentrated flow	nville, FL	w concentrate m Channel De <u>Vel. (fps)</u> 9.27	d flow esgin.	3	<u>ı.)</u> min.	

St. Johns River Power Park CURVE NUMBER & TIME OF CONCENTRATION REVISED AREA B DRAINAGE BASINS								
Basin Description45.93 ac.								
<u>CN:</u>								
	<u>Ac.</u>	Land Cover	Soil Type	SCS CN	<u>%</u>	Weight %		
	5.60	Final Cover (Open Space - Good)	С	74	94.4%	70		
	0.07	Perimeter Road (Impervious)	-	98	1.2%	1		
	0.26	Pond/Pool (Water)	-	98	4.4% 100.0%	4		
Total:	5.93	<u>OK</u>		Weighted S		75		
*The second s	•	lculated using the TR-55 velocity vs. slope c	riteria for shallo					
The remainin Mannings of (	).24 - Dense Gr			m Channel De	sgin.			
*The remainin *Mannings of ( *P2-yr,24-hr (i	).24 - Dense Gr n.) - NOAA Pred	asses sipitation Frequency Data Server for Jacksor		m Channel De	sgin.			
The remainin Mannings of ( P2-yr,24-hr (i Overland	0.24 - Dense Gr n.) - NOAA Pred Mannings n	asses sipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	ville, FL	m Channel De	sgin.			
The remainin Mannings of ( P2-yr,24-hr (i	0.24 - Dense Gr n.) - NOAA Pred Mannings n	asses sipitation Frequency Data Server for Jacksor	ville, FL	m Channel De	sgin.			
The remainin Mannings of ( P2-yr,24-hr (i Overland	0.24 - Dense Gr n.) - NOAA Pred Mannings n	asses sipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	ville, FL	m Channel De <u>Vel. (fps)</u>	sgin.	<u>Time (min.)</u>		
The remainin Mannings of ( P2-yr,24-hr (i Overland	0.24 - Dense Gr n.) - NOAA Pred Mannings n 0.24	asses sipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	ville, FL		sgin.	<u>Time (min.)</u> 20		
The remainin Mannings of ( P2-yr,24-hr (i Overland	0.24 - Dense Gr n.) - NOAA Pred Mannings n 0.24 <u>Dist. (ft)</u>	asses cipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.) 4.74 0.05	ville, FL		sgin.			
The remainin Mannings of ( P2-yr,24-hr (i Overland	0.24 - Dense Gr n.) - NOAA Pred Mannings n 0.24 <u>Dist. (ft)</u> <u>300</u>	asses cipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.) 4.74 0.05 Sheet Flow	ville, FL	<u>Vel. (fps)</u>	sgin.	20		

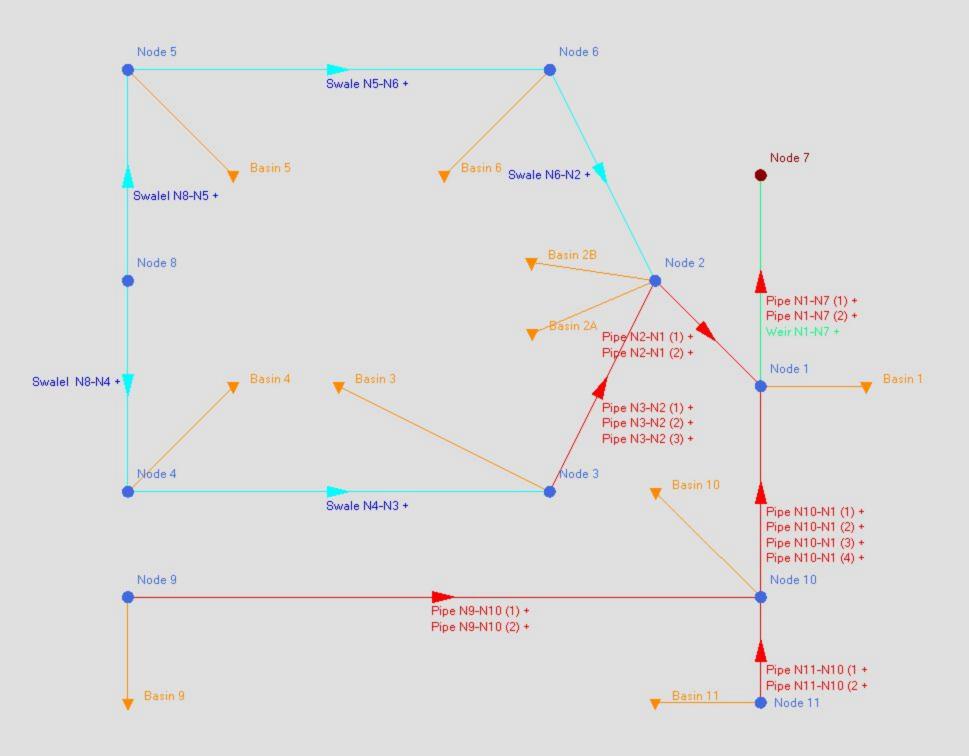
St. Johns River Power Park CURVE NUMBER & TIME OF CONCENTRATION REVISED AREA B DRAINAGE BASINS								
Basin Description55.21 ac.								
<u>CN:</u>								
	Ac.	Land Cover	<u>Soil Type</u>	SCS CN	<u>%</u>	Weight %		
	4.95	Final Cover (Open Space - Good)	С	74	95.0%	70		
	0.09	Perimeter Road (Impervious)	-	98	1.7%	2		
	0.17	Pond/Pool (Water)	-	98	3.3% 100.0%	3		
Total:	5.21	<u>OK</u>		Weighted S	SCS CN =	75		
<b>Tc:</b> First Time of	Concentration s	egment less than 300-ft was calculated using	g the TR-55 for	mula for sheet	t flow			
First Time of The second s The remainin	egment was ca g segment was	Iculated using the TR-55 velocity vs. slope cr calculated using average channel flow veloci	iteria for shallo	w concentrate	d flow			
First Time of The second s The remainings of (	egment was ca g segment was 0.24 - Dense Gr	Iculated using the TR-55 velocity vs. slope cr calculated using average channel flow veloci asses	iteria for shallo ty obtained froi	w concentrate	d flow			
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Pred	Iculated using the TR-55 velocity vs. slope cr calculated using average channel flow veloci asses cipitation Frequency Data Server for Jackson	iteria for shallo ty obtained froi	w concentrate	d flow			
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Preo Mannings n	Iculated using the TR-55 velocity vs. slope cr calculated using average channel flow veloci asses	iteria for shallo ity obtained froi ville, FL	w concentrate	d flow			
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i Overland	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Pred Mannings n 0.24	Iculated using the TR-55 velocity vs. slope or calculated using average channel flow veloci rasses cipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	iteria for shallo ity obtained froi ville, FL	w concentrate	d flow	Time (min.)		
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i Overland	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Preo Mannings n	Iculated using the TR-55 velocity vs. slope or calculated using average channel flow veloci rasses cipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	iteria for shallo ity obtained froi ville, FL	w concentrate m Channel De	d flow	<u>Time (min.)</u> 20		
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i Overland	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Pred Mannings n 0.24 <u>Dist. (ft)</u>	Iculated using the TR-55 velocity vs. slope or calculated using average channel flow velocitances   casses   cipitation Frequency Data Server for Jackson   P2-yr,24-hr (in.)   Slope (ft./ft.)   4.74	iteria for shallo ity obtained froi ville, FL	w concentrate m Channel De	d flow			
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i Overland	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Pred Mannings n 0.24 <u>Dist. (ft)</u> 300	Iculated using the TR-55 velocity vs. slope or calculated using average channel flow velocitasses   cipitation Frequency Data Server for Jackson   P <sub>2-yr,24-hr</sub> (in.)   Slope (ft./ft.)   4.74   0.05	iteria for shallo ity obtained froi ville, FL	w concentrate m Channel De <u>Vel. (fps)</u>	d flow	20		
First Time of The second s The remainin Mannings of ( P2-yr,24-hr (i Overland	egment was ca g segment was 0.24 - Dense Gr n.) - NOAA Pred Mannings n 0.24 <u>Dist. (ft)</u> 300 30	Iculated using the TR-55 velocity vs. slope or calculated using average channel flow velocitasses   cipitation Frequency Data Server for Jackson   P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)   4.74 0.05   Sheet Flow   Shallow concentrated flow	iteria for shallo ity obtained froi ville, FL	w concentrate m Channel De <u>Vel. (fps)</u> <u>3.61</u>	d flow	20 0		

St. Johns River Power Park CURVE NUMBER & TIME OF CONCENTRATION REVISED AREA B DRAINAGE BASINS								
Basin Description66.21 ac.								
<u>CN:</u>								
	Ac.	Land Cover	<u>Soil Type</u>	SCS CN	%	<u>Weight %</u>		
	5.85	Final Cover (Open Space - Good)	С	74	94.2%	70		
	0.19	Perimeter Road (Impervious)	-	98	3.1%	3		
	0.17	Pond/Pool (Water)	-	98	2.7% 100.0%	3		
Total:	6.21	<u>OK</u>		Weighted S		75		
Tc: First Time of	Concentration s	egment less than 300-ft was calculated using	g the TR-55 for	mula for sheet	t flow			
First Time of The second s The remainin	segment was ca	culated using the TR-55 velocity vs. slope cr calculated using average channel flow veloci	iteria for shallo	w concentrate	d flow			
First Time of The second s The remainin Mannings of	segment was ca ng segment was 0.24 - Dense Gr	culated using the TR-55 velocity vs. slope cr calculated using average channel flow veloci	iteria for shallo ty obtained froi	w concentrate	d flow			
First Time of The second s The remainin Mannings of P2-yr,24-hr (i	segment was ca ng segment was 0.24 - Dense Gr in.) - NOAA Preo	lculated using the TR-55 velocity vs. slope cr calculated using average channel flow veloci asses cipitation Frequency Data Server for Jackson	iteria for shallo ty obtained froi	w concentrate	d flow			
First Time of The second s The remainin Mannings of P2-yr,24-hr (i	segment was ca ng segment was 0.24 - Dense Gr in.) - NOAA Preo Mannings n	lculated using the TR-55 velocity vs. slope cr calculated using average channel flow veloci asses cipitation Frequency Data Server for Jackson	iteria for shallo ty obtained froi ville, FL	w concentrate	d flow			
First Time of The second s The remainin Mannings of P2-yr,24-hr (i Overland	segment was ca ng segment was 0.24 - Dense Gr in.) - NOAA Preo Mannings n	culated using the TR-55 velocity vs. slope or calculated using average channel flow veloci asses cipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	iteria for shallo ty obtained froi ville, FL	w concentrate	d flow	<u>Time (min.)</u>		
First Time of The second s The remainin Mannings of P2-yr,24-hr (i Overland	segment was ca ng segment was 0.24 - Dense Gr in.) - NOAA Preo Mannings n 0.24	culated using the TR-55 velocity vs. slope or calculated using average channel flow veloci asses cipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	iteria for shallo ty obtained froi ville, FL	w concentrate m Channel De	d flow	<u>Time (min.)</u> 20		
First Time of The second s The remainin Mannings of P2-yr,24-hr (i Overland	segment was ca ng segment was 0.24 - Dense Gr in.) - NOAA Preo Mannings n 0.24 <u>Dist. (ft)</u>	Iculated using the TR-55 velocity vs. slope or calculated using average channel flow veloci asses sipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.) 4.74 0.05	iteria for shallo ty obtained froi ville, FL	w concentrate m Channel De	d flow			
First Time of The second s The remainin Mannings of P2-yr,24-hr (i Overland	segment was ca ng segment was 0.24 - Dense Gr in.) - NOAA Pred Mannings n 0.24 <u>Dist. (ft)</u> 300	Iculated using the TR-55 velocity vs. slope or calculated using average channel flow velocitasses   cipitation Frequency Data Server for Jackson   P <sub>2-yr,24-hr</sub> (in.)   Slope (ft./ft.)   4.74   0.05	iteria for shallo ty obtained froi ville, FL	w concentrate m Channel De <u>Vel. (fps)</u>	d flow	20		
First Time of The second s The remainin Mannings of P2-yr,24-hr (i Overland	segment was ca ng segment was 0.24 - Dense Gr in.) - NOAA Pred Mannings n 0.24 <u>Dist. (ft)</u> 300 0	Iculated using the TR-55 velocity vs. slope or calculated using average channel flow velocitasses   cipitation Frequency Data Server for Jackson   P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)   4.74 0.05   Sheet Flow   Shallow concentrated flow	iteria for shallo ty obtained froi ville, FL	w concentrate m Channel De <u>Vel. (fps)</u> <u>3.61</u>	d flow	20 0		

St. Johns River Power Park CURVE NUMBER & TIME OF CONCENTRATION REVISED AREA B DRAINAGE BASINS								
Basin Description 9 10.94 ac.								
<u>CN:</u>								
	<u>Ac.</u>	Land Cover	Soil Type	SCS CN	%	Weight %		
	9.72	Tie-in Areas (Open Space - Good)	С	74	88.8%	66		
	1.22	Perimeter Road (Impervious)	-	98	11.2%	11		
	0.00	Pond/Pool (Water)	-	98	0.0% 100.0%	0		
Total:	10.94	<u>OK</u>		Weighted S		77		
*The remaining *Mannings of 0 *P2-yr,24-hr (in	g segment was 0.24 - Dense G 0.) - NOAA Pre	Iculated using the TR-55 velocity vs. slope cri calculated using average channel flow velocit rasses cipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.)	y obtained fro					
Flow		4.74 0.005	j					
	Dist. (ft)			<u>Vel. (fps)</u>		<u>Time (min.)</u>		
	<u>300</u>	Sheet Flow		<u> </u>		49		
	300							
	375	Shallow concentrated flow		1.14		5		
				1.14 4.60		5 0		
Fotal:	375	Shallow concentrated flow Open channel flow						

St. Johns River Power Park CURVE NUMBER & TIME OF CONCENTRATION REVISED AREA B DRAINAGE BASINS							
Basin Desc	ription	10 (Pond B)		8.56	ac.		
<u>CN:</u>							
	Ac.	Land Cover	Soil Type	SCS CN	%	Weight %	
	<u>Ac.</u> 2.57	Tie-in Areas (Open Space - Good)	С	74	30.0%	22	
	0.00	Perimeter Road (Impervious)	-	98	0.0%	0	
	5.99	Pond/Pool (Water)	-	98	70.0% 100.0%	69	
Total:	8.56	<u>OK</u>		Weighted S		91	
*The second s *The remainin *Mannings of *P2-yr,24-hr (i	segment was ca g segment was 0.24 - Dense G n.) - NOAA Pre Mannings n	segment less than 300-ft was calculated using local local local during the TR-55 velocity vs. slope cri calculated using average channel flow velocit rasses cipitation Frequency Data Server for Jacksony P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.) 4.74 0.05	teria for shallo y obtained fro /ille, FL	w concentrate	d flow		
						, .	
	<u>Dist. (ft)</u>			<u>Vel. (fps)</u>		<u>Time (min.</u>	)
	70	Sheet Flow		0.04		6	
	0	Shallow concentrated flow		3.61		0	
<del>.</del>	0	Open channel flow		4.60		0	
Fotal: 70 Time of Concentration = 6 m		min.					

St. Johns River Power Park CURVE NUMBER & TIME OF CONCENTRATION REVISED AREA B DRAINAGE BASINS							
Basin Desc	ription	11		3.53	ac.		
<u>CN:</u>							
	<u>Ac.</u>	Land Cover	<u>Soil Type</u>	SCS CN	<u>%</u>	Weight %	, D
	2.61	Tie-in Areas (Open Space - Good)	C	74	73.9%	55	_
	0.92	Perimeter Road (Impervious)	-	98	26.1%	26	
	0.00	Pond/Pool (Water)	-	98	0.0% 100.0%	0	
Total:	3.53	<u>OK</u>		Weighted S		80	
*The second s *The remaining *Mannings of ( *P2-yr,24-hr (ii	egment was ca g segment was 0.24 - Dense G n.) - NOAA Pre Mannings n	segment less than 300-ft was calculated using ilculated using the TR-55 velocity vs. slope cri calculated using average channel flow velocit rasses cipitation Frequency Data Server for Jackson P <sub>2-yr,24-hr</sub> (in.) Slope (ft./ft.) 4.74 0.05	teria for shallo ty obtained fro ville, FL	w concentrate	d flow		
	Dist. (ft)			Vel. (fps)		<u>Time (min</u>	
	<u>70</u>	Sheet Flow		<u>voi. (ipoj</u>		<u>11110 (11111</u> 6	<u>.,</u>
	0	Shallow concentrated flow		3.61		0	
	0	Open channel flow		4.60		0	
Total:	70			1.00		Ŭ	
			min.				



Simple Basin: Basin 1	
Scenario:	SJRPP AREA B 2021
Node:	Node 1
Hydrograph Method:	NRCS Unit Hydrograph
Infiltration Method:	Curve Number
Time of Concentration:	8.0000 min
Max Allowable Q:	999999.00 cfs
Time Shift:	0.0000 hr
Unit Hydrograph:	Uh256
Peaking Factor:	256.0
Area:	15.9800 ac
Curve Number:	97.0
% Impervious:	0.00
% DCIA:	0.00
% Direct:	0.00
Rainfall Name:	
Comment:	

1		Deale	Deele	1/	2
Simp	le	Basin	Basin		J

Scenario:	SJRPP AREA B 2021
Node:	Node 10
Hydrograph Method:	NRCS Unit Hydrograph
Infiltration Method:	Curve Number
Time of Concentration:	6.0000 min
Max Allowable Q:	999999.00 cfs
Time Shift:	0.0000 hr
Unit Hydrograph:	Uh256
Peaking Factor:	256.0
Area:	8.5600 ac
Curve Number:	91.0
% Impervious:	0.00
% DCIA:	0.00
% Direct:	0.00
Rainfall Name:	

Comment:

#### Simple Basin: Basin 11

Scenario:	SJRPP AREA B 2021
Node:	Node 11
Hydrograph Method:	NRCS Unit Hydrograph
Infiltration Method:	Curve Number
Time of Concentration:	6.0000 min
Max Allowable Q:	999999.00 cfs

Time Shift:	0.0000 hr
Unit Hydrograph:	UH256
Peaking Factor:	256.0
Area:	3.5300 ac
Curve Number:	80.0
% Impervious:	0.00
% DCIA:	0.00
% Direct:	0.00
Rainfall Name:	

#### Comment:

Simple Basin: Basin 2A	
Scenario:	SJRPP AREA B 2021
Node:	Node 2
Hydrograph Method:	NRCS Unit Hydrograph
Infiltration Method:	Curve Number
Time of Concentration:	21.0000 min
Max Allowable Q:	999999.00 cfs
Time Shift:	0.0000 hr
Unit Hydrograph:	Uh256
Peaking Factor:	256.0
Area:	6.0700 ac
Curve Number:	77.0
% Impervious:	0.00
% DCIA:	0.00
% Direct:	0.00
Rainfall Name:	

Comment:

-				
Simple Basin: Basin 2B				
Scenario:	SJRPP AREA B 2021			
Node:	Node 2			
Hydrograph Method:	NRCS Unit Hydrograph			
Infiltration Method:	Curve Number			
Time of Concentration:	21.0000 min			
Max Allowable Q:	999999.00 cfs			
Time Shift:	0.0000 hr			
Unit Hydrograph:	Uh256			
Peaking Factor:	256.0			
Area:	4.2200 ac			
Curve Number:	78.0			
% Impervious:	0.00			
% DCIA:	0.00			

% Direct: 0.00

Rainfall Name:

Comment:

Simple Basin: Basin 3	
Scenario:	SJRPP AREA B 2021
Node:	Node 3
Hydrograph Method:	NRCS Unit Hydrograph
Infiltration Method:	Curve Number
Time of Concentration:	6.0000 min
Max Allowable Q:	999999.00 cfs
Time Shift:	0.0000 hr
Unit Hydrograph:	Uh256
Peaking Factor:	256.0
Area:	3.7100 ac
Curve Number:	81.0
% Impervious:	0.00
% DCIA:	0.00
% Direct:	0.00
Rainfall Name:	

Comment:

Simple Basin: Basin 4	
Scenario:	SJRPP AREA B 2021
Node:	Node 4
Hydrograph Method:	NRCS Unit Hydrograph
Infiltration Method:	Curve Number
Time of Concentration:	21.0000 min
Max Allowable Q:	999999.00 cfs
Time Shift:	0.0000 hr
Unit Hydrograph:	Uh256
Peaking Factor:	256.0
Area:	5.9300 ac
Curve Number:	75.0
% Impervious:	0.00
% DCIA:	0.00
% Direct:	0.00
Rainfall Name:	

Comment:

Simple Basin: Basin 5	
Scenario:	SJRPP AREA B 2021
Node:	Node 5
Hydrograph Method:	NRCS Unit Hydrograph
Infiltration Method:	Curve Number
Time of Concentration:	21.0000 min
Max Allowable Q:	999999.00 cfs
Time Shift:	0.0000 hr
Unit Hydrograph:	Uh256
Peaking Factor:	256.0
Area:	5.2100 ac
Curve Number:	75.0
% Impervious:	0.00
% DCIA:	0.00
% Direct:	0.00
Rainfall Name:	
Comment:	

Comment:

#### Simple Basin: Basin 6

Scenario:	SJRPP AREA B 2021
Node:	Node 6
Hydrograph Method:	NRCS Unit Hydrograph
Infiltration Method:	Curve Number
Time of Concentration:	20.0000 min
Max Allowable Q:	999999.00 cfs
Time Shift:	0.0000 hr
Unit Hydrograph:	Uh256
Peaking Factor:	256.0
Area:	6.2100 ac
Curve Number:	75.0
% Impervious:	0.00
% DCIA:	0.00
% Direct:	0.00
Rainfall Name:	

Comment:

#### Simple Basin: Basin 9

Scenario:	SJRPP AREA B 2021
Node:	Node 9
Hydrograph Method:	NRCS Unit Hydrograph
Infiltration Method:	Curve Number
Time of Concentration:	55.0000 min
Max Allowable Q:	999999.00 cfs

Time Shift:	0.0000 hr
Unit Hydrograph:	Uh256
Peaking Factor:	256.0
Area:	10.9400 ac
Curve Number:	77.0
% Impervious:	0.00
% DCIA:	0.00
% Direct:	0.00
Rainfall Name:	

#### Comment:

#### Node: Node 1

Scenario:SJRPP AREA B 2021Type:Stage/AreaBase Flow:0.00 cfsInitial Stage:7.40 ftWarning Stage:11.00 ft

Stage [ft]	Area [ac]	Area [ft2]
3.00	9.9000	431244
4.00	10.1800	443441
5.00	10.5600	459994
6.00	10.9300	476111
7.00	11.7900	513572
7.50	12.3700	538837
8.00	12.9600	564538
8.50	13.1800	574121
9.00	13.3900	583268
10.00	13.8200	601999
11.00	14.2600	621166

#### Comment:

#### Node: Node 10

Scenario:	SJRPP AREA B 2021
Type:	Stage/Area
Base Flow:	0.00 cfs
Initial Stage:	7.90 ft
Warning Stage:	13.00 ft

Stage [ft]	Area [ac]	Area [ft2]
-1.00	0.4300	18731
0.00	0.8800	38333
1.00	1.1700	50965

Stage [ft]	Area [ac]	Area [ft2]
2.00	1.4500	63162
3.00	1.7500	76230
4.00	2.0400	88862
5.00	2.3400	101930
6.00	2.6400	114998
7.00	2.9900	130244
8.00	3.3700	146797
9.00	3.7900	165092
10.00	4.2800	186437
11.00	4.8100	209524
12.00	5.3000	230868
13.00	5.9900	260924

Comment:

#### Node: Node 11

Scenario:	SJRPP AREA B 2021
Type:	Stage/Area
Base Flow:	0.00 cfs
Initial Stage:	11.50 ft
Warning Stage:	14.00 ft

Stage [ft]	Area [ac]	Area [ft2]
11.50	0.0463	2017
12.00	0.2203	9596
12.50	0.4260	18555
13.00	0.6739	29354
13.50	0.9113	39697
14.00	1.1633	50672
14.50	1.4245	62049

#### Comment:

#### Node: Node 2

Scenario:	SJRPP AREA B 2021
Туре:	Stage/Area
Base Flow:	0.00 cfs
Initial Stage:	9.00 ft
Warning Stage:	12.60 ft

Stage [ft]	Area [ac]	Area [ft2]
9.00	0.1500	6534
10.00	0.5300	23087
11.00	0.8400	36590

Stage [ft]	Area [ac]	Area [ft2]
12.00	1.1200	48787
Comment:		

	Base Flow: Initial Stage: Warning Stage:	0.00 cfs 11.00 ft 15.00 ft	
Stage [ft]		Area [ac]	Area [ft2]
	11.00	0.0100	436
	12.00	0.0100	436
	13.00	0.1100	4792
	14.00	0.2900	12632
	15.00	0.5300	23087
	16.00	0.8800	38333

Scenario: SJRPP AREA B 2021 Type: Stage/Area

#### Comment:

Node: Node 3

Node: Node 4

Scenario:	SJRPP AREA B 2021
Type:	Stage/Area
Base Flow:	0.00 cfs
Initial Stage:	18.65 ft
Warning Stage:	20.65 ft

#### Comment:

#### Node: Node 5

Scenario:	SJRPP AREA B 2021
Type:	Stage/Area
Base Flow:	0.00 cfs
Initial Stage:	16.07 ft
Warning Stage:	18.07 ft

Comment:

#### Node: Node 6

Scenario:	SJRPP AREA B 2021
Type:	Stage/Area
Base Flow:	0.00 cfs
Initial Stage:	11.73 ft
Warning Stage:	13.73 ft

#### Comment:

#### Node: Node 7

Scenario:	SJRPP AREA B 2021
Type:	Time/Stage
Base Flow:	0.00 cfs
Initial Stage:	7.00 ft
Warning Stage:	7.00 ft
Boundary Stage:	

Year	Month	Day	Hour	Stage [ft]
0	0	0	0.0000	7.00
0	0	0	999.0000	7.00

Comment:

#### Node: Node 8

Scenario:	SJRPP AREA B 2021
Type:	Stage/Area
Base Flow:	0.00 cfs
Initial Stage:	18.80 ft
Warning Stage:	20.80 ft

#### Comment: High Point at Channel.

#### Node: Node 9

Scenario:	SJRPP AREA B 2021
Туре:	Stage/Area
Base Flow:	0.00 cfs
Initial Stage:	11.50 ft
Warning Stage:	14.00 ft

Stage [ft]	Area [ac]	Area [ft2]
11.50	0.0700	3049
12.00	0.5200	22651
12.50	1.4200	61855
13.00	2.7000	117612
13.50	4.1900	182516
14.00	5.6800	247421
14.50	7.0500	307098
	-	

Comment:

Pipe Link: Pipe N1-N7 (1)		Upstream		Down	Downstream	
Scenario:	SJRPP AREA B	Invert:	7.48 ft	Invert:	7.46 ft	
	2021	Manning's N:	0.0110	Manning's N:	0.0110	
From Node:	Node 1	Geometry	y: Circular	Geometr	y: Circular	
To Node:	Node 7	Max Depth:	0.67 ft	Max Depth:	0.67 ft	
Link Count:	1			Bottom Clip		
Flow Direction:	Both	Default:	0.00 ft	Default:	0.00 ft	
Damping:	0.0000 ft	Op Table:		Op Table:		
Length:	44.00 ft	Ref Node:		Ref Node:		
FHWA Code:	3	Manning's N:	0.0110	Manning's N:	0.0110	
Entr Loss Coef:	0.00			Top Clip		
Exit Loss Coef:	1.00	Default:	0.00 ft	Default:	0.00 ft	
Bend Loss Coef:	0.00	Op Table:		Op Table:		
Bend Location:	0.00 dec	Ref Node:		Ref Node:		
Energy Switch:	Energy	Manning's N:	0.0110	Manning's N:	0.0110	
Comment:						

Pipe Link: Pipe N1-N7 (2)		Upstream		Dowr	Downstream	
Scenario:	SJRPP AREA B	Invert:	7.48 ft	Invert:	7.48 ft	
	2021	Manning's N:	0.0110	Manning's N:	0.0110	
From Node:	Node 1	Geometry	y: Circular	Geomet	ry: Circular	
To Node:	Node 7	Max Depth:	0.67 ft	Max Depth:	0.67 ft	
Link Count:	1			Bottom Clip		
Flow Direction:	Both	Default:	0.00 ft	Default:	0.00 ft	
Damping:	0.0000 ft	Op Table:		Op Table:		
Length:	44.00 ft	Ref Node:		Ref Node:		
FHWA Code:	3	Manning's N:	0.0110	Manning's N:	0.0110	
Entr Loss Coef:	0.00			Top Clip		
Exit Loss Coef:	1.00	Default:	0.00 ft	Default:	0.00 ft	
Bend Loss Coef:	0.00	Op Table:		Op Table:		
Bend Location:	0.00 dec	Ref Node:		Ref Node:		
Energy Switch:	Energy	Manning's N:	0.0110	Manning's N:	0.0110	
Comment:						

Pipe Link: Pipe N10-N1 (1)		Upstream		Dow	Downstream	
Scenario:	SJRPP AREA B	Invert:	7.95 ft	Invert	: 7.72 ft	
	2021	Manning's N:	0.0120	Manning's N	: 0.0120	
From Node:	Node 10	Geometry: V	ertical Ellipse	Geometry:	Vertical Ellipse	
To Node:	Node 1	Max Depth:	3.17 ft	Max Depth	: 3.17 ft	
Link Count:	1			Bottom Clip		
Flow Direction:	Both	Default:	0.00 ft	Default	: 0.00 ft	
Damping:	0.0000 ft	Op Table:		Op Table	:	
Length:	44.00 ft	Ref Node:		Ref Node	:	
FHWA Code:	35	Manning's N:	0.0120	Manning's N	: 0.0120	
Entr Loss Coef:	0.00			Top Clip		
Exit Loss Coef:	1.00	Default:	0.00 ft	Default	: 0.00 ft	
Bend Loss Coef:	0.00	Op Table:		Op Table	:	
Bend Location:	0.00 dec	Ref Node:		Ref Node	:	
Energy Switch:	Energy	Manning's N:	0.0120	Manning's N	: 0.0120	
Comment:						

Pipe Link: Pipe N10-N1 (2)		Upstream		Dowi	Downstream	
Scenario:	SJRPP AREA B	Invert:	7.91 ft	Invert:	7.71 ft	
	2021	Manning's N:	0.0120	Manning's N:	0.0120	
From Node:	Node 10	Geometry: V	ertical Ellipse	Geometry:	Vertical Ellipse	
To Node:	Node 1	Max Depth:	3.17 ft	Max Depth:	3.17 ft	
Link Count:	1			Bottom Clip		
Flow Direction:	Both	Default:	0.00 ft	Default:	0.00 ft	
Damping:	0.0000 ft	Op Table:		Op Table:		
Length:	44.00 ft	Ref Node:		Ref Node:		
FHWA Code:	35	Manning's N:	0.0120	Manning's N:	0.0120	
Entr Loss Coef:	0.00			Top Clip		
Exit Loss Coef:	1.00	Default:	0.00 ft	Default:	0.00 ft	
Bend Loss Coef:	0.00	Op Table:		Op Table:		
Bend Location:	0.00 dec	Ref Node:		Ref Node:		
Energy Switch:	Energy	Manning's N:	0.0120	Manning's N:	0.0120	
Comment:						

Pipe Link: Pipe N10-N1 (3)		Upstream		Dowr	Downstream	
Scenario:	SJRPP AREA B	Invert:	7.90 ft	Invert:	7.76 ft	
	2021	Manning's N:	0.0120	Manning's N:	0.0120	
From Node:	Node 10	Geometry: V	ertical Ellipse	Geometry: '	/ertical Ellipse	
To Node:	Node 1	Max Depth:	3.17 ft	Max Depth:	3.17 ft	
Link Count:	1			Bottom Clip		
Flow Direction:	Both	Default:	0.00 ft	Default:	0.00 ft	
Damping:	0.0000 ft	Op Table:		Op Table:		
Length:	44.00 ft	Ref Node:		Ref Node:		
FHWA Code:	35	Manning's N:	0.0120	Manning's N:	0.0120	
Entr Loss Coef:	0.00		Top Clip			

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Exit Loss Coef:	1.00	Default:	0.00 ft	Default:	0.00 ft
Bend Loss Coef:	0.00	Op Table:		Op Table:	
Bend Location:	0.00 dec	Ref Node:		Ref Node:	
Energy Switch:	Energy	Manning's N:	0.0120	Manning's N:	0.0120
Comment:					

Pipe Link: Pipe N10-N1 (4)		Upstream		Downstream	
Scenario:			7.92 ft	Invert:	7.72 ft
	2021	Manning's N:	0.0120	Manning's N:	0.0120
From Node:	Node 10	Geometry: V	ertical Ellipse	Geometry: \	/ertical Ellipse
To Node:	Node 1	Max Depth:	3.17 ft	Max Depth:	3.17 ft
Link Count:	1			Bottom Clip	
Flow Direction:	Both	Default:	0.00 ft	Default:	0.00 ft
Damping:	0.0000 ft	Op Table:		Op Table:	
Length:	44.00 ft	Ref Node:		Ref Node:	
FHWA Code:	35	Manning's N:	0.0120	Manning's N:	0.0120
Entr Loss Coef:	0.00			Top Clip	
Exit Loss Coef:	1.00	Default:	0.00 ft	Default:	0.00 ft
Bend Loss Coef:	0.00	Op Table:		Op Table:	
Bend Location:	0.00 dec	Ref Node:		Ref Node:	
Energy Switch:	Energy	Manning's N:	0.0120	Manning's N:	0.0120
Comment:					

Pipe Link: Pipe N11-N10 (1		Upst	Upstream		Downstream	
Scenario:	SJRPP AREA B	Invert:	11.24 ft	Invert	: 10.23 ft	
	2021	Manning's N:	0.0120	Manning's N	. 0.0120	
From Node:	Node 11	Geometry: V	ertical Ellipse	Geometry:	Vertical Ellipse	
To Node:	Node 10	Max Depth:	3.17 ft	Max Depth	: 3.17 ft	
Link Count:	1			Bottom Clip		
Flow Direction:	Both	Default:	0.00 ft	Default	: 0.00 ft	
Damping:	0.0000 ft	Op Table:		Op Table	:	
Length:	68.00 ft	Ref Node:		Ref Node	:	
FHWA Code:	35	Manning's N:	0.0120	Manning's N	. 0.0120	
Entr Loss Coef:	0.00			Top Clip		
Exit Loss Coef:	1.00	Default:	0.00 ft	Default	: 0.00 ft	
Bend Loss Coef:	0.00	Op Table:		Op Table	:	
Bend Location:	0.00 dec	Ref Node:		Ref Node	:	
Energy Switch:	Energy	Manning's N:	0.0120	Manning's N	. 0.0120	
Comment:	57	<u> </u>	-			

Pipe Link: Pipe N11-N10 (2	Upstream	Downstream	
Scenario: SJRPP AREA B	Invert: 11.25 ft	Invert: 10.23 ft	

	2021	Manning's N:	0.0120	Manning's N:	0.0120
From Node:	Node 11	Geometry: V	ertical Ellipse	Geometry: \	/ertical Ellipse
To Node:	Node 10	Max Depth:	3.17 ft	Max Depth:	3.17 ft
Link Count:	1			Bottom Clip	
Flow Direction:	Both	Default:	0.00 ft	Default:	0.00 ft
Damping:	0.0000 ft	Op Table:		Op Table:	
Length:	68.00 ft	Ref Node:		Ref Node:	
FHWA Code:	35	Manning's N:	0.0120	Manning's N:	0.0120
Entr Loss Coef:	0.00			Top Clip	
Exit Loss Coef:	1.00	Default:	0.00 ft	Default:	0.00 ft
Bend Loss Coef:	0.00	Op Table:		Op Table:	
Bend Location:	0.00 dec	Ref Node:		Ref Node:	
Energy Switch:	Energy	Manning's N:	0.0120	Manning's N:	0.0120
Comment:					

Pipe Link: Pipe N2-N	1 (1)	Upst	ream	Dowr	nstream
Scenario:	SJRPP AREA B	Invert:	8.47 ft	Invert:	7.45 ft
	2021	Manning's N:	0.0120	Manning's N:	0.0120
From Node:	Node 2	Geometry: V	ertical Ellipse	Geometry: \	/ertical Ellipse
To Node:	Node 1	Max Depth:	3.17 ft	Max Depth:	3.17 ft
Link Count:	1			Bottom Clip	
Flow Direction:	Both	Default:	0.00 ft	Default:	0.00 ft
Damping:	0.0000 ft	Op Table:		Op Table:	
Length:	64.00 ft	Ref Node:		Ref Node:	
FHWA Code:	35	Manning's N:	0.0120	Manning's N:	0.0120
Entr Loss Coef:	0.00			Top Clip	
Exit Loss Coef:	1.00	Default:	0.00 ft	Default:	0.00 ft
Bend Loss Coef:	0.00	Op Table:		Op Table:	
Bend Location:	0.00 dec	Ref Node:		Ref Node:	
Energy Switch:	Energy	Manning's N:	0.0120	Manning's N:	0.0120
Comment:					

Pipe Link: Pipe N2-N1 (2)		Upst	Upstream		Downstream	
Scenario:	SJRPP AREA B	Invert:	8.43 ft	Invert:	7.46 ft	
	2021	Manning's N:	0.0120	Manning's N:	0.0120	
From Node:	Node 2	Geometry: V	ertical Ellipse	Geometry: \	Vertical Ellipse	
To Node:	Node 1	Max Depth:	3.17 ft	Max Depth:	3.17 ft	
Link Count:	1			Bottom Clip		
Flow Direction:	Both	Default:	0.00 ft	Default:	0.00 ft	
Damping:	0.0000 ft	Op Table:		Op Table:		
Length:	64.00 ft	Ref Node:		Ref Node:		
FHWA Code:	35	Manning's N:	0.0120	Manning's N:	0.0120	
Entr Loss Coef:	0.00			Top Clip		
Exit Loss Coef:	1.00	Default:	0.00 ft	Default:	0.00 ft	
Bend Loss Coef:	0.00	Op Table:		Op Table:		

Bend Location:	0.00 dec	Ref Node:		Ref Node:	
Energy Switch:	Energy	Manning's N:	0.0120	Manning's N:	0.0120
Comment:					

Pipe Link: Pipe N3-N	Pipe Link: Pipe N3-N2 (1)		Upstream		stream
Scenario:	SJRPP AREA B	Invert:	11.95 ft	Invert:	11.93 ft
	2021	Manning's N:	0.0120	Manning's N:	0.0120
From Node:	Node 3	Geometry: V	ertical Ellipse	Geometry: \	/ertical Ellipse
To Node:	Node 2	Max Depth:	3.17 ft	Max Depth:	3.17 ft
Link Count:	1			Bottom Clip	
Flow Direction:	Both	Default:	0.00 ft	Default:	0.00 ft
Damping:	0.0000 ft	Op Table:		Op Table:	
Length:	66.00 ft	Ref Node:		Ref Node:	
FHWA Code:	35	Manning's N:	0.0120	Manning's N:	0.0120
Entr Loss Coef:	0.00			Top Clip	
Exit Loss Coef:	1.00	Default:	0.00 ft	Default:	0.00 ft
Bend Loss Coef:	0.00	Op Table:		Op Table:	
Bend Location:	0.00 dec	Ref Node:		Ref Node:	
Energy Switch:	Energy	Manning's N:	0.0120	Manning's N:	0.0120
Comment:					

Pipe Link: Pipe N3-N2 (2)		Upstream		Dow	Downstream	
Scenario:	SJRPP AREA B	Invert:	12.05 ft	Invert	11.86 ft	
	2021	Manning's N:	0.0120	Manning's N	0.0120	
From Node:	Node 3	Geometry: V	ertical Ellipse	Geometry:	Vertical Ellipse	
To Node:	Node 2	Max Depth:	3.17 ft	Max Depth	3.17 ft	
Link Count:	1			Bottom Clip		
Flow Direction:	Both	Default:	0.00 ft	Default	0.00 ft	
Damping:	0.0000 ft	Op Table:		Op Table		
Length:	66.00 ft	Ref Node:		Ref Node		
FHWA Code:	35	Manning's N:	0.0120	Manning's N	0.0120	
Entr Loss Coef:	0.00			Top Clip		
Exit Loss Coef:	1.00	Default:	0.00 ft	Default	0.00 ft	
Bend Loss Coef:	0.00	Op Table:		Op Table		
Bend Location:	0.00 dec	Ref Node:		Ref Node		
Energy Switch:	Energy	Manning's N:	0.0120	Manning's N	0.0120	
Comment:						

Pipe Link: Pipe N3-N2 (3)		Upstream	Downstream
Scenario:	SJRPP AREA B	Invert: 12.10 ft	Invert: 11.86 ft
	2021	Manning's N: 0.0120	Manning's N: 0.0120
From Node:	Node 3	Geometry: Vertical Ellipse	Geometry: Vertical Ellipse

### SJRPP Area B ROROCS ICPR Input Report

To Node:	Node 2	Max Depth:	3.17 ft	Max Depth:	3.17 ft
Link Count:	1			Bottom Clip	
Flow Direction:	Both	Default:	0.00 ft	Default:	0.00 ft
Damping:	0.0000 ft	Op Table:		Op Table:	
Length:	66.00 ft	Ref Node:		Ref Node:	
FHWA Code:	35	Manning's N:	0.0120	Manning's N:	0.0120
Entr Loss Coef:	0.00			Top Clip	
Exit Loss Coef:	1.00	Default:	0.00 ft	Default:	0.00 ft
Bend Loss Coef:	0.00	Op Table:		Op Table:	
Bend Location:	0.00 dec	Ref Node:		Ref Node:	
Energy Switch:	Energy	Manning's N:	0.0120	Manning's N:	0.0120
Comment:					

Pipe Link: Pipe N9-N	10 (1)	Upst	ream	Dow	nstream
Scenario:	SJRPP AREA B	Invert:	11.24 ft	Invert	: 10.23 ft
	2021	Manning's N:	0.0120	Manning's N	. 0.0120
From Node:	Node 9	Geometry: V	ertical Ellipse	Geometry:	Vertical Ellipse
To Node:	Node 10	Max Depth:	3.17 ft	Max Depth	: 3.17 ft
Link Count:	1			Bottom Clip	
Flow Direction:	Both	Default:	0.00 ft	Default	: 0.00 ft
Damping:	0.0000 ft	Op Table:		Op Table	:
Length:	66.00 ft	Ref Node:		Ref Node	:
FHWA Code:	35	Manning's N:	0.0120	Manning's N	. 0.0120
Entr Loss Coef:	0.00			Top Clip	
Exit Loss Coef:	1.00	Default:	0.00 ft	Default	: 0.00 ft
Bend Loss Coef:	0.00	Op Table:		Op Table	:
Bend Location:	0.00 dec	Ref Node:		Ref Node	:
Energy Switch:	Energy	Manning's N:	0.0120	Manning's N	0.0120
Comment:					

Pipe Link: Pipe N9-N	10 (2)	Upst	ream	Dowr	nstream
Scenario:	SJRPP AREA B	Invert:	11.24 ft	Invert:	10.23 ft
	2021	Manning's N:	0.0120	Manning's N:	0.0120
From Node:	Node 9	Geometry: V	ertical Ellipse	Geometry:	Vertical Ellipse
To Node:	Node 10	Max Depth:	3.17 ft	Max Depth:	3.17 ft
Link Count:	1			Bottom Clip	
Flow Direction:	Both	Default:	0.00 ft	Default:	0.00 ft
Damping:	0.0000 ft	Op Table:		Op Table:	
Length:	66.00 ft	Ref Node:		Ref Node:	
FHWA Code:	35	Manning's N:	0.0120	Manning's N:	0.0120
Entr Loss Coef:	0.00			Top Clip	
Exit Loss Coef:	1.00	Default:	0.00 ft	Default:	0.00 ft
Bend Loss Coef:	0.00	Op Table:		Op Table:	
Bend Location:	0.00 dec	Ref Node:		Ref Node:	
Energy Switch:	Energy	Manning's N:	0.0120	Manning's N:	0.0120

## Comment:

Channel Link: Swale	N4-N3	Upst	ream	Down	istream
Scenario:	SJRPP AREA B	Invert:	18.65 ft	Invert:	17.34 ft
	2021	Manning's N:	0.0300	Manning's N:	0.0300
From Node:	Node 4	Geometry:	Trapezoidal	Geometry:	Trapezoidal
To Node:	Node 3	Max Depth:	9980.35 ft	Max Depth:	9981.66 ft
Link Count:	1	Extrapolation:	Normal	Extrapolation:	Normal
Flow Direction:	Both	Bottom Width:	4.00 ft	Bottom Width:	8.00 ft
Damping:	0.0000 ft	Left Slope:	3.000 (h:v)	Left Slope:	3.000 (h:v)
Length:	230.00 ft	Right Slope:	3.000 (h:v)	Right Slope:	3.000 (h:v)
Contraction Coef:	0.10			Bottom Clip	
Expansion Coef:	0.30	Default:	0.00 ft	Default:	0.00 ft
Entr Loss Coef:	0.00	Op Table:		Op Table:	
Exit Loss Coef:	0.00	Ref Node:		Ref Node:	
Bend Loss Coef:	0.00	Manning's N:	0.0300	Manning's N:	0.0300
Bend Location:	0.00 dec			Top Clip	
Energy Switch:	Energy	Default:	0.00 ft	Default:	0.00 ft
		Op Table:		Op Table:	
		Ref Node:		Ref Node:	
		Manning's N:	0.0300	Manning's N:	0.0300
Comment:		~		0	

Channel Link: Swale	N5-N6	Upst	ream	Down	stream
Scenario:	SJRPP AREA B	Invert:	16.07 ft	Invert:	11.73 ft
	2021	Manning's N:	0.0300	Manning's N:	0.0300
From Node:	Node 5	Geometry:	Trapezoidal	Geometry:	Trapezoidal
To Node:	Node 6	Max Depth:	9982.93 ft	Max Depth:	9987.27 ft
Link Count:	1	Extrapolation:	Normal	Extrapolation:	Normal
Flow Direction:	Both	Bottom Width:	8.00 ft	Bottom Width:	10.00 ft
Damping:	0.0000 ft	Left Slope:	3.000 (h:v)	Left Slope:	3.000 (h:v)
Length:	870.00 ft	Right Slope:	3.000 (h:v)	Right Slope:	3.000 (h:v)
Contraction Coef:	0.10			Bottom Clip	
Expansion Coef:	0.30	Default:	0.00 ft	Default:	0.00 ft
Entr Loss Coef:	0.00	Op Table:		Op Table:	
Exit Loss Coef:	0.00	Ref Node:		Ref Node:	
Bend Loss Coef:	0.00	Manning's N:	0.0300	Manning's N:	0.0300
Bend Location:	0.00 dec			Top Clip	
Energy Switch:	Energy	Default:	0.00 ft	Default:	0.00 ft
		Op Table:		Op Table:	
		Ref Node:		Ref Node:	
		Manning's N:	0.0300	Manning's N:	0.0300
Comment:					

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### SJRPP Area B ROROCS ICPR Input Report

Channel Link: Swale	N6-N2	Upst	ream	Down	stream
Scenario:	SJRPP AREA B	Invert:	11.73 ft	Invert:	9.84 ft
	2021	Manning's N:	0.0300	Manning's N:	0.0300
From Node:	Node 6	Geometry:	Trapezoidal	Geometry:	Trapezoidal
To Node:	Node 2	Max Depth:	9987.27 ft	Max Depth:	9989.16 ft
Link Count:	1	Extrapolation:	Normal	Extrapolation:	Normal
Flow Direction:	Both	Bottom Width:	10.00 ft	Bottom Width:	10.00 ft
Damping:	0.0000 ft	Left Slope:	3.000 (h:v)	Left Slope:	3.000 (h:v)
Length:	400.00 ft	Right Slope:	3.000 (h:v)	Right Slope:	3.000 (h:v)
Contraction Coef:	0.10			Bottom Clip	
Expansion Coef:	0.30	Default:	0.00 ft	Default:	0.00 ft
Entr Loss Coef:	0.00	Op Table:		Op Table:	
Exit Loss Coef:	0.00	Ref Node:		Ref Node:	
Bend Loss Coef:	0.00	Manning's N:	0.0300	Manning's N:	0.0300
Bend Location:	0.00 dec			Top Clip	
Energy Switch:	Energy	Default:	0.00 ft	Default:	0.00 ft
		Op Table:		Op Table:	
		Ref Node:		Ref Node:	
		Manning's N:	0.0300	Manning's N:	0.0300
Comment:					

Channel Link: Swalel	N8-N4	Upst	ream	Down	stream
Scenario:	SJRPP AREA B	Invert:	18.80 ft	Invert:	18.65 ft
	2021	Manning's N:	0.0300	Manning's N:	0.0300
From Node:	Node 8	Geometry:	Trapezoidal	Geometry:	Trapezoidal
To Node:	Node 4	Max Depth:	9980.20 ft	Max Depth:	9980.35 ft
Link Count:	1	Extrapolation:	Normal	Extrapolation:	Normal
Flow Direction:	Both	Bottom Width:	4.00 ft	Bottom Width:	4.00 ft
Damping:	0.0000 ft	Left Slope:	3.000 (h:v)	Left Slope:	3.000 (h:v)
Length:	30.00 ft	Right Slope:	3.000 (h:v)	Right Slope:	3.000 (h:v)
Contraction Coef:	0.00			Bottom Clip	
Expansion Coef:	0.00	Default:	0.00 ft	Default:	0.00 ft
Entr Loss Coef:	0.00	Op Table:		Op Table:	
Exit Loss Coef:	0.00	Ref Node:		Ref Node:	
Bend Loss Coef:	0.00	Manning's N:	0.0300	Manning's N:	0.0300
Bend Location:	0.00 dec			Top Clip	
Energy Switch:	Energy	Default:	0.00 ft	Default:	0.00 ft
		Op Table:		Op Table:	
		Ref Node:		Ref Node:	
		Manning's N:	0.0300	Manning's N:	0.0300
Comment:					

Channel Link: Swalel N8-N5		Upstream		Downstream	
Scenario:	SJRPP AREA B	Invert:	18.80 ft	Invert:	16.07 ft
	2021	Manning's N:	0.0300	Manning's N:	0.0300

## SJRPP Area B ROROCS ICPR Input Report

From Node:	Node 8	Geometry:	Trapezoidal	Geometry	Trapezoidal
To Node:	Node 5	Max Depth:	9980.20 ft	Max Depth:	9982.93 ft
Link Count:	1	Extrapolation:	Normal	Extrapolation:	Normal
Flow Direction:	Both	Bottom Width:	4.00 ft	Bottom Width:	8.00 ft
Damping:	0.0000 ft	Left Slope:	3.000 (h:v)	Left Slope:	3.000 (h:v)
Length:	550.00 ft	Right Slope:	3.000 (h:v)	Right Slope:	3.000 (h:v)
Contraction Coef:	0.10			Bottom Clip	
Expansion Coef:	0.30	Default:	0.00 ft	Default:	0.00 ft
Entr Loss Coef:	0.00	Op Table:		Op Table:	
Exit Loss Coef:	0.00	Ref Node:		Ref Node:	
Bend Loss Coef:	0.00	Manning's N:	0.0300	Manning's N:	0.0300
Bend Location:	0.00 dec			Top Clip	
Energy Switch:	Energy	Default:	0.00 ft	Default:	0.00 ft
		Op Table:		Op Table:	
		Ref Node:		Ref Node:	
		Manning's N:	0.0300	Manning's N:	0.0300
Comment:					

Weir Link: Weir N1-N7			
Scenario:	SJRPP AREA B 2021	Bottor	m Clip
From Node:	Node 1	Default:	0.00 ft
To Node:	Node 7	Op Table:	
Link Count:	1	Ref Node:	
Flow Direction:	Both	Тор	Clip
Damping:	0.0000 ft	Default:	0.00 ft
Weir Type:	Broad Crested Vertical	Op Table:	
Geometry Type:	Trapezoidal	Ref Node:	
Invert:	8.36 ft	Discharge (	Coefficients
Control Elevation:	8.36 ft	Weir Default:	3.200
Max Depth:	9999.00 ft	Weir Table:	
Extrapolation Method:	Normal Projection	Orifice Default:	0.600
Bottom Width:	24.00 ft	Orifice Table:	
Left Slope:	3.000 (h:v)		
Right Slope:	3.000 (h:v)		
Comment:			

Simulation: 25-24				
Scenario:	SJRPP AREA B 2021			
Run Date/Time:	10/4/2021 7:34:53 PM			
Program Version:	ICPR4 4.07.08			
			-	
		General		
Run Mode:	Normal			
	Year	Month	Day	Hour [hr]

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Start Time:	0	0	0	0.0000
End Time:	0	0	0	72.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000	_	
Max Calculation Time:		60.0000		
		Output Time Increments	5	
Hydr	rology			
ear	Month	Day	Hour [hr]	Time Increment [min]
	0	0	0.0000	15.000
Surface	Hydraulics			
ear	Month	Day	Hour [hr]	Time Increment [min]
	0	0	0.0000	15.000
Resta Save Restart:	art File False			
Suvo Rostart.				
		Resources & Lookup Tabl	es	
Resc	ources		Lookup	Tables
Rainfall Folder:	ICPR3		Boundary Stage Set:	
Unit Hydrograph Folder:	ICPR3		Extern Hydrograph Set: Curve Number Set:	
			Green-Ampt Set:	
			Vertical Layers Set:	
			Impervious Set:	
		Tolerances & Options		
Time Marching:	SAOR		IA Recovery Time:	24.0000 hr
Max Iterations:	6 0 E dee			
Over-Relax Weight Fact:	0.5 dec			
dZ Tolerance:	0.0010 ft		Smp/Man Basin Rain Opt:	Global
Max dZ:	1.0000 ft			
Link Optimizer Tol:	0.0001 ft		Rainfall Name: Rainfall Amount:	Flmod 8.99 in
Edge Length Option:	Automatic		Storm Duration:	24.0000 hr
			Dflt Damping (1D):	0.0050 ft

Energy Switch (1D): Energy

Comment:

## SJRPP Area B ROROCS ICPR Nodal Max Report

Scenario	Sim	Node Name	Warning Stage [ft]	Maximum Stage [ft]	Maximum Inflow Rate [cfs]
SJRPP AREA B 2021	25-24	Node 1	11	8.97	140.15
SJRPP AREA B 2021	25-24	Node 2	12.6	12.18	95.8
SJRPP AREA B 2021	25-24	Node 3	15	13.8	28.9
SJRPP AREA B 2021	25-24	Node 4	20.65	19.44	17.74
SJRPP AREA B 2021	25-24	Node 5	18.07	16.78	22.11
SJRPP AREA B 2021	25-24	Node 6	13.73	12.77	40.5
SJRPP AREA B 2021	25-24	Node 7	7	7	42.02
SJRPP AREA B 2021	25-24	Node 8	20.8	19.3	6.62
SJRPP AREA B 2021	25-24	Node 9	14	12.6	19.7
SJRPP AREA B 2021	25-24	Node 10	13	9.14	67.2
SJRPP AREA B 2021	25-24	Node 11	14	12.57	18.73

Scenario	Sim	Relative Time [hrs]	Precipitation Volume [ac_ft]	Rainfall Excess Volume [ac_ft]	Stored Volume (Flow Based) [ac_ft]	Total Inflow Volume [ac_ft]	Total Outflow Volume [ac_ft]
SJRPP AREA B 2021	25-24	0	0	0	0	0	0
SJRPP AREA B 2021	25-24	0.2667	0.17	0	0.17	0.17	0
SJRPP AREA B 2021	25-24	0.5167	0.33	0	0.33	0.33	0
SJRPP AREA B 2021	25-24	0.75	0.47	0	0.47	0.47	0
SJRPP AREA B 2021	25-24	1	0.63	0.01	0.62	0.63	0.01
SJRPP AREA B 2021	25-24	1.25	0.8	0.02	0.78	0.8	0.02
SJRPP AREA B 2021	25-24	1.5167	0.99	0.04	0.95	0.99	0.04
SJRPP AREA B 2021	25-24	1.7667	1.16	0.06	1.1	1.16	0.06
SJRPP AREA B 2021	25-24	2.0167	1.33	0.08	1.25	1.33	0.08
SJRPP AREA B 2021	25-24	2.2667	1.51	0.1	1.41	1.51	0.1
SJRPP AREA B 2021	25-24	2.5167	1.7	0.13	1.56	1.7	0.13
SJRPP AREA B 2021	25-24	2.7667	1.88	0.17	1.71	1.88	0.17
SJRPP AREA B 2021	25-24	3.0167	2.06	0.2	1.86	2.06	0.2
SJRPP AREA B 2021	25-24	3.2667	2.26	0.24	2.02	2.26	0.24
SJRPP AREA B 2021	25-24	3.5167	2.46	0.28	2.18	2.46	0.28
SJRPP AREA B 2021	25-24	3.7667	2.66	0.33	2.33	2.66	0.33
SJRPP AREA B 2021	25-24	4.0167	2.86	0.38	2.49	2.86	0.38
SJRPP AREA B 2021	25-24	4.2667	3.09	0.43	2.66	3.09	0.43
SJRPP AREA B 2021	25-24	4.5167	3.31	0.49	2.82	3.31	0.49
SJRPP AREA B 2021	25-24	4.7667	3.53	0.55	2.99	3.53	0.55
SJRPP AREA B 2021	25-24	5.0167	3.76	0.61	3.15	3.76	0.61
SJRPP AREA B 2021	25-24	5.2667	4	0.68	3.32	4	0.68
SJRPP AREA B 2021	25-24	5.5167	4.23	0.75	3.48	4.23	0.75
SJRPP AREA B 2021	25-24	5.7667	4.47	0.83	3.64	4.47	0.83
SJRPP AREA B 2021	25-24	6.0167	4.71	0.92	3.79	4.71	0.92
SJRPP AREA B 2021	25-24	6.2667	4.99	1.02	3.97	4.99	1.02
SJRPP AREA B 2021	25-24	6.5167	5.26	1.13	4.13	5.26	1.13
SJRPP AREA B 2021	25-24	6.7667	5.54	1.24	4.3	5.54	1.24
SJRPP AREA B 2021	25-24	7.0167	5.82	1.36	4.46	5.82	1.36
SJRPP AREA B 2021	25-24	7.2667	6.13	1.51	4.63	6.13	1.51
SJRPP AREA B 2021	25-24	7.5167	6.45	1.65	4.8	6.45	1.65

Scenario	Sim	Relative Time [hrs]	Precipitation Volume [ac_ft]	Rainfall Excess Volume [ac_ft]	Stored Volume (Flow Based) [ac_ft]	Total Inflow Volume [ac_ft]	Total Outflow Volume [ac_ft]
SJRPP AREA B 2021	25-24	7.7667	6.77	1.81	4.96	6.77	1.81
SJRPP AREA B 2021	25-24	8.0167	7.09	1.97	5.12	7.09	1.97
SJRPP AREA B 2021	25-24	8.2667	7.46	2.16	5.3	7.46	2.16
SJRPP AREA B 2021	25-24	8.5	7.8	2.34	5.46	7.8	2.34
SJRPP AREA B 2021	25-24	8.75	8.22	2.58	5.65	8.22	2.58
SJRPP AREA B 2021	25-24	9	8.64	2.82	5.83	8.64	2.82
SJRPP AREA B 2021	25-24	9.25	9.09	3.08	6.01	9.09	3.08
SJRPP AREA B 2021	25-24	9.5	9.54	3.35	6.19	9.54	3.35
SJRPP AREA B 2021	25-24	9.75	10.07	3.68	6.39	10.07	3.68
SJRPP AREA B 2021	25-24	10	10.59	4.02	6.58	10.59	4.02
SJRPP AREA B 2021	25-24	10.25	11.25	4.45	6.81	11.25	4.45
SJRPP AREA B 2021	25-24	10.5	11.91	4.89	7.02	11.91	4.89
SJRPP AREA B 2021	25-24	10.75	12.76	5.48	7.28	12.76	5.48
SJRPP AREA B 2021	25-24	11	13.6	6.08	7.52	13.6	6.08
SJRPP AREA B 2021	25-24	11.25	14.5	6.73	7.77	14.5	6.73
SJRPP AREA B 2021	25-24	11.5	16.23	8.04	8.19	16.23	8.04
SJRPP AREA B 2021	25-24	11.75	22.13	12.8	9.34	22.13	12.8
SJRPP AREA B 2021	25-24	12	32	21.41	10.58	32	21.41
SJRPP AREA B 2021	25-24	12.25	36.05	25.1	10.95	36.05	25.1
SJRPP AREA B 2021	25-24	12.5	37.9	26.8	11.1	37.9	26.8
SJRPP AREA B 2021	25-24	12.75	39.01	27.82	11.19	39.01	27.82
SJRPP AREA B 2021	25-24	13	39.9	28.65	11.25	39.9	28.65
SJRPP AREA B 2021	25-24	13.25	40.64	29.33	11.31	40.64	29.33
SJRPP AREA B 2021	25-24	13.5	41.38	30.02	11.36	41.38	30.02
SJRPP AREA B 2021	25-24	13.75	41.96	30.56	11.4	41.96	30.56
SJRPP AREA B 2021	25-24	14	42.54	31.1	11.43	42.54	31.1
SJRPP AREA B 2021	25-24	14.25	43.04	31.57	11.47	43.04	31.57
SJRPP AREA B 2021	25-24	14.5	43.54	32.04	11.5	43.54	32.04
SJRPP AREA B 2021	25-24	14.75	43.96	32.44	11.53	43.96	32.44
SJRPP AREA B 2021	25-24	15	44.38	32.83	11.55	44.38	32.83
SJRPP AREA B 2021	25-24	15.25	44.78	33.2	11.58	44.78	33.2

Scenario	Sim	Relative Time [hrs]	Precipitation Volume [ac_ft]	Rainfall Excess Volume [ac_ft]	Stored Volume (Flow Based) [ac_ft]	Total Inflow Volume [ac_ft]	Total Outflow Volume [ac_ft]
SJRPP AREA B 2021	25-24	15.5	45.17	33.57	11.6	45.17	33.57
SJRPP AREA B 2021	25-24	15.75	45.52	33.9	11.62	45.52	33.9
SJRPP AREA B 2021	25-24	16	45.86	34.22	11.64	45.86	34.22
SJRPP AREA B 2021	25-24	16.25	46.18	34.52	11.66	46.18	34.52
SJRPP AREA B 2021	25-24	16.5	46.49	34.81	11.68	46.49	34.81
SJRPP AREA B 2021	25-24	16.75	46.78	35.09	11.69	46.78	35.09
SJRPP AREA B 2021	25-24	17	47.07	35.36	11.71	47.07	35.36
SJRPP AREA B 2021	25-24	17.25	47.36	35.63	11.73	47.36	35.63
SJRPP AREA B 2021	25-24	17.5	47.65	35.91	11.74	47.65	35.91
SJRPP AREA B 2021	25-24	17.75	47.89	36.13	11.76	47.89	36.13
SJRPP AREA B 2021	25-24	18	48.13	36.36	11.77	48.13	36.36
SJRPP AREA B 2021	25-24	18.25	48.39	36.61	11.78	48.39	36.61
SJRPP AREA B 2021	25-24	18.5	48.65	36.86	11.8	48.65	36.86
SJRPP AREA B 2021	25-24	18.75	48.86	37.06	11.81	48.86	37.06
SJRPP AREA B 2021	25-24	19	49.07	37.25	11.82	49.07	37.25
SJRPP AREA B 2021	25-24	19.25	49.31	37.48	11.83	49.31	37.48
SJRPP AREA B 2021	25-24	19.5	49.55	37.7	11.84	49.55	37.7
SJRPP AREA B 2021	25-24	19.75	49.76	37.9	11.86	49.76	37.9
SJRPP AREA B 2021	25-24	20	49.97	38.1	11.87	49.97	38.1
SJRPP AREA B 2021	25-24	20.25	50.15	38.28	11.88	50.15	38.28
SJRPP AREA B 2021	25-24	20.5	50.34	38.45	11.88	50.34	38.45
SJRPP AREA B 2021	25-24	20.75	50.52	38.63	11.89	50.52	38.63
SJRPP AREA B 2021	25-24	21	50.71	38.8	11.9	50.71	38.8
SJRPP AREA B 2021	25-24	21.25	50.89	38.98	11.91	50.89	38.98
SJRPP AREA B 2021	25-24	21.5	51.08	39.16	11.92	51.08	39.16
SJRPP AREA B 2021	25-24	21.75	51.26	39.33	11.93	51.26	39.33
SJRPP AREA B 2021	25-24	22	51.45	39.51	11.94	51.45	39.51
SJRPP AREA B 2021	25-24	22.25	51.63	39.68	11.95	51.63	39.68
SJRPP AREA B 2021	25-24	22.5	51.82	39.86	11.96	51.82	39.86
SJRPP AREA B 2021	25-24	22.7667	51.98	40.02	11.97	51.98	40.02
SJRPP AREA B 2021	25-24	23.0167	52.14	40.17	11.97	52.14	40.17

Scenario	Sim	Relative Time [hrs]	Precipitation Volume [ac_ft]	Rainfall Excess Volume [ac_ft]	Stored Volume (Flow Based) [ac_ft]	Total Inflow Volume [ac_ft]	Total Outflow Volume [ac_ft]
SJRPP AREA B 2021	25-24	23.2667	52.3	40.32	11.98	52.3	40.32
SJRPP AREA B 2021	25-24	23.5167	52.46	40.47	11.99	52.46	40.47
SJRPP AREA B 2021	25-24	23.7667	52.59	40.59	11.99	52.59	40.59
SJRPP AREA B 2021	25-24	24.0167	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	24.2667	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	24.5167	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	24.7667	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	25.0167	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	25.2667	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	25.5167	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	25.7667	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	26.0167	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	26.2667	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	26.5167	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	26.7667	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	27.0167	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	27.2667	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	27.5167	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	27.7667	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	28.0167	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	28.2667	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	28.5167	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	28.7667	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	29.0167	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	29.2667	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	29.5167	52.71	40.71	12	52.71	40.71
SJRPP AREA B 2021	25-24	29.7667	52.71	40.71	12	52.71	40.71



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